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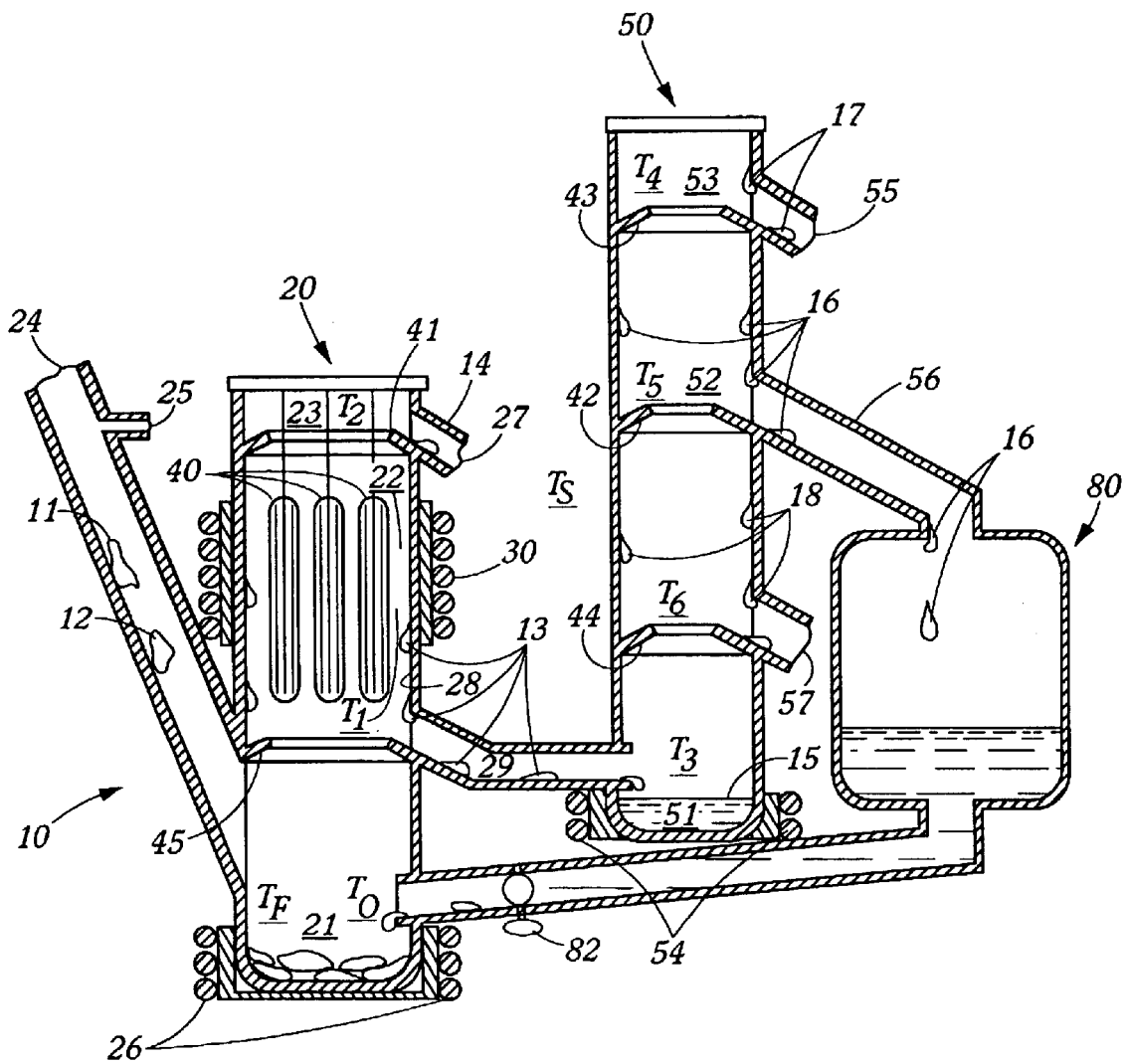


FIG. 1

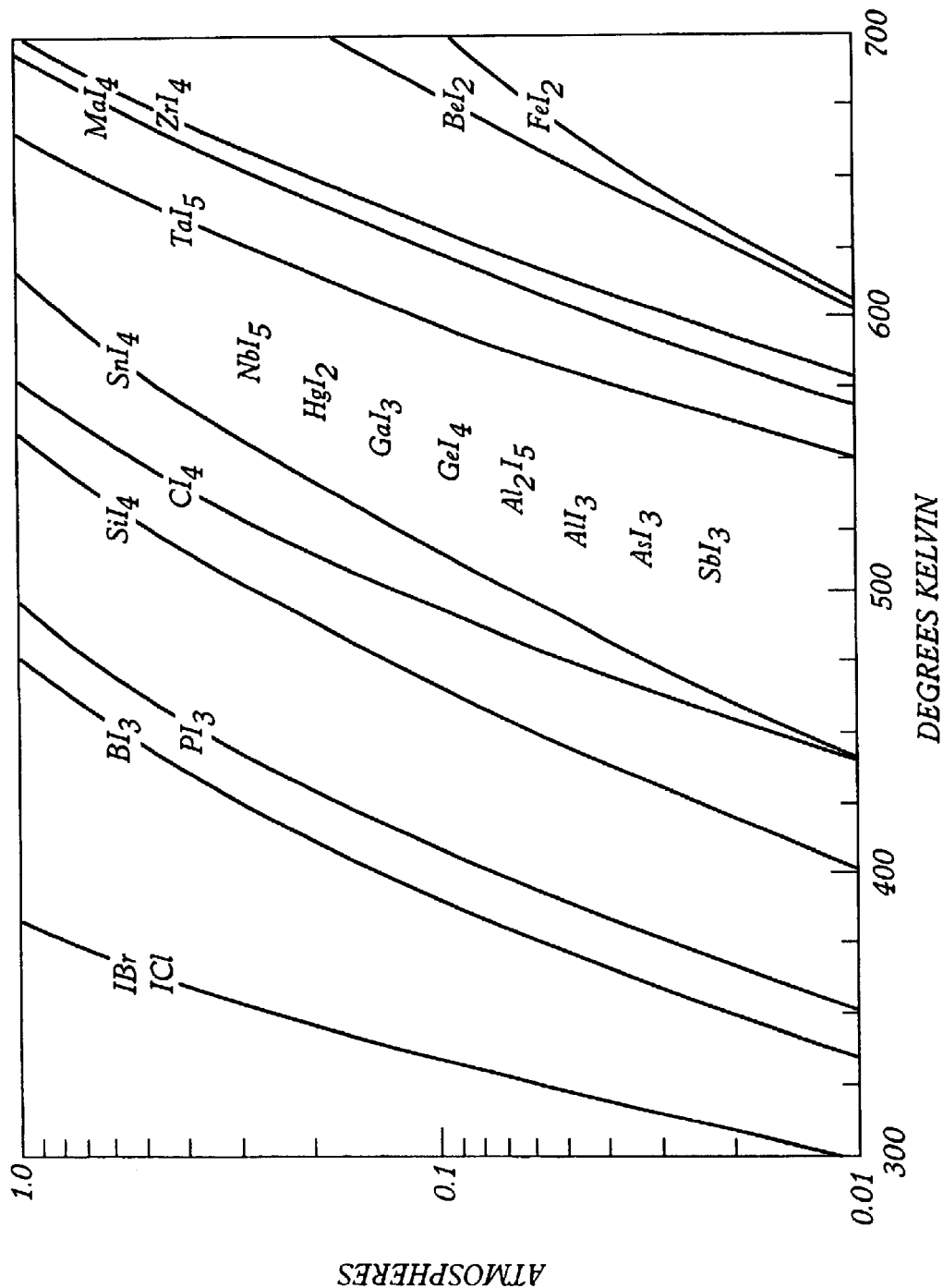


FIG. 2

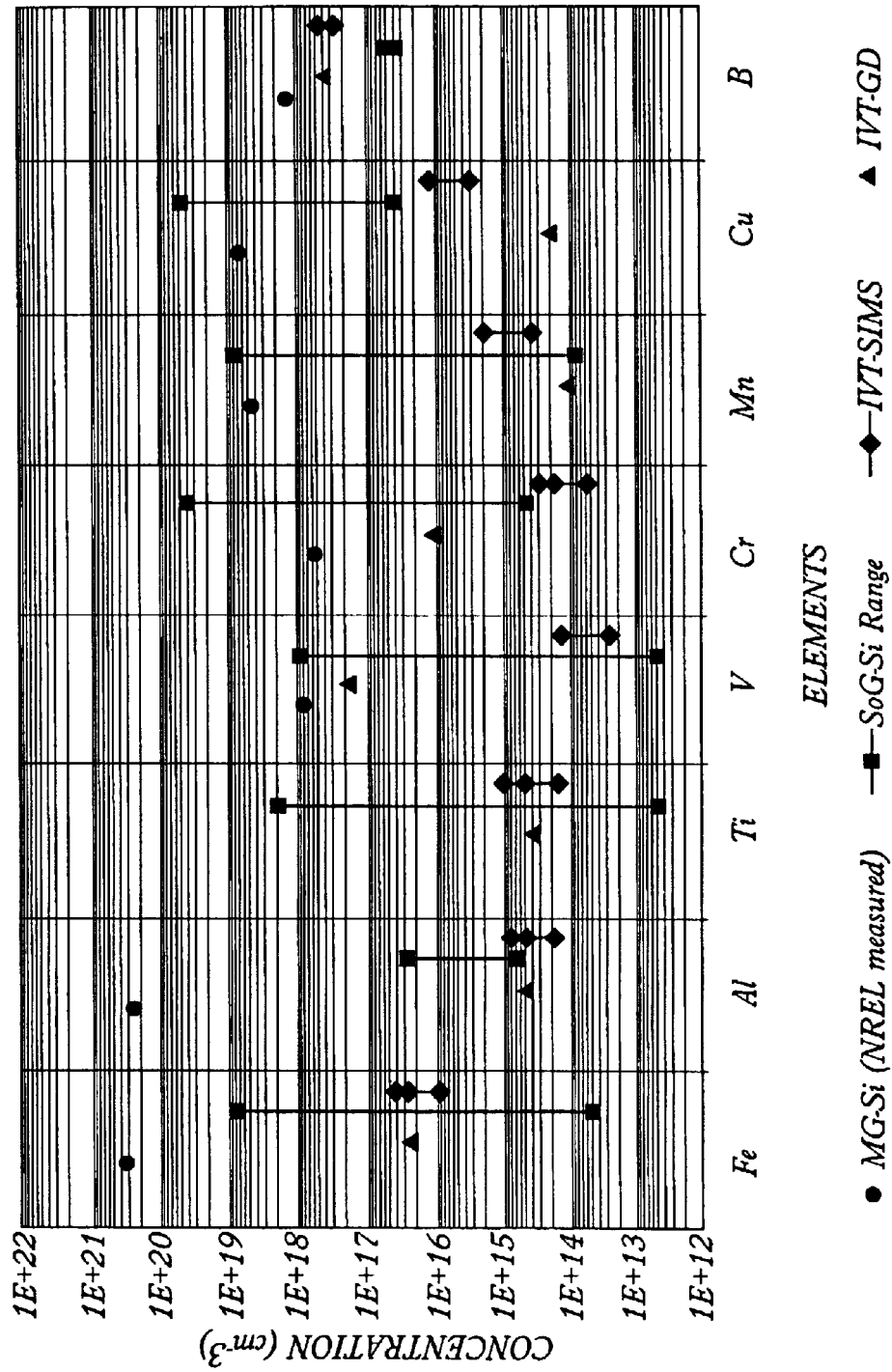


FIG. 3

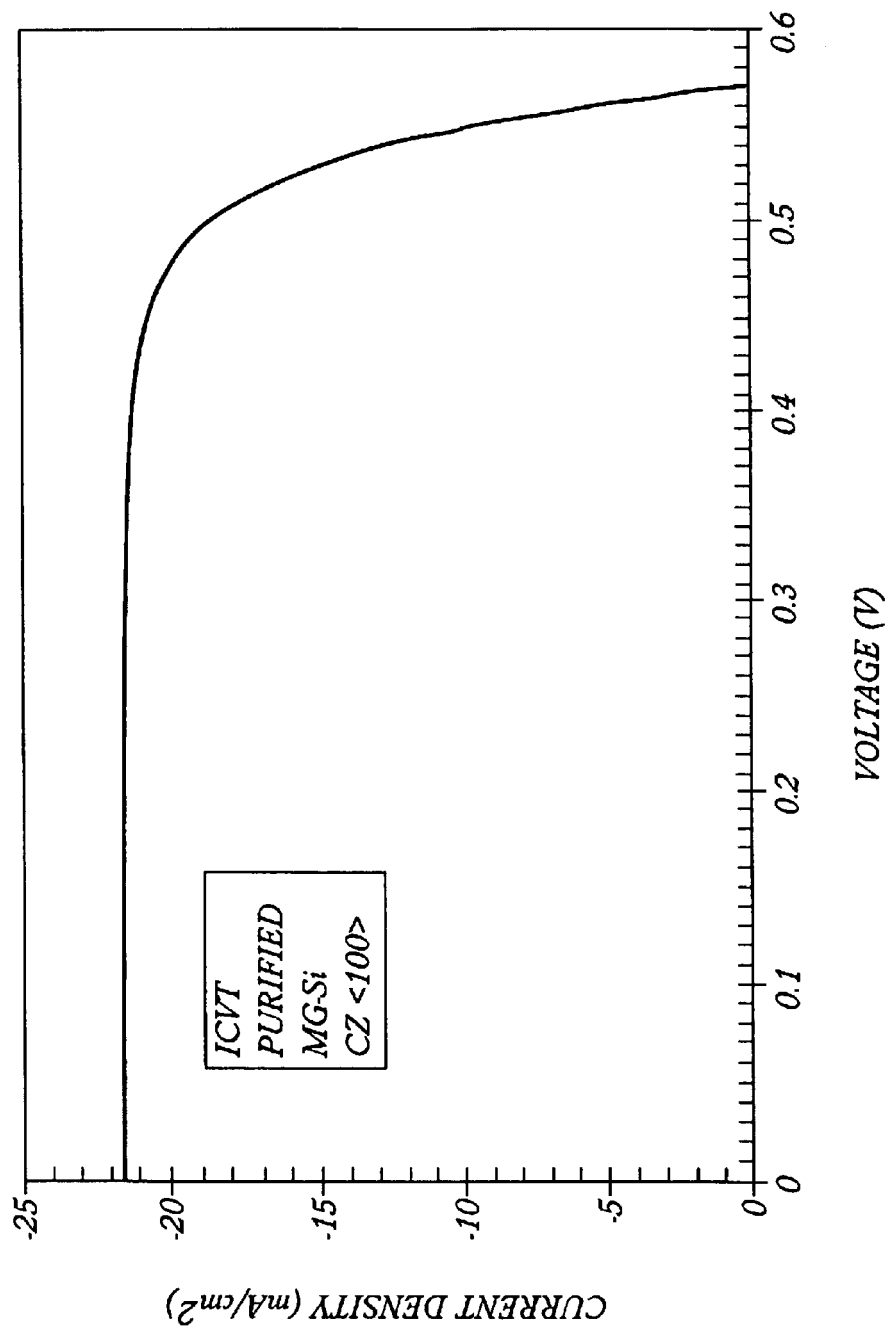


FIG. 4

PURIFIED SILICON PRODUCTION SYSTEM**CROSS-REFERENCE TO RELATED PATENT APPLICATION**

This patent application is a divisional application of Ser. No. 09/941,490, filed Aug. 28, 2001 now U.S. Pat. No. 6,468,886, which is a continuation-in-part of U.S. patent application Ser. No. 09/334,166, filed on Jun. 15, 1999, now U.S. Pat. No. 6,281,098.

The United States Government has rights in this invention pursuant to Contract No. DE-AC36-99GO10337 between the United States Department of Energy and the National Renewable Energy Laboratory, a division of Midwest Research Institute.

FIELD OF INVENTION

The present invention pertains generally to producing silicon feedstock for the semiconductor industry, and more specifically, to purifying metallurgical-grade silicon by means of iodine chemical vapor transport to produce pure silicon feedstock for use in fabricating photovoltaic and other semiconductor devices.

BACKGROUND OF INVENTION

About 85% of the photovoltaic modules sold annually are made from silicon. Manufacturers have repeatedly expressed concern about the future supply of low-cost feedstock as this market continues to grow at a rate exceeding 30% each year. Recent reports project that demand for silicon from the electronics industry will exceed the current supply levels by a factor of 2 to 4 within the next decade. This projection does not represent a fundamental material shortage problem because the technology, quartzite, and coke needed to make feedstock are in abundant supply. Rather, the issue is how best to supply the required feedstock with the requisite purity (~99.999%) to manufacturers at an acceptable cost. Several methods exist for the manufacture of silicon feedstock that meet at least a portion of the manufacturing sector's requirements, including the widely used silicon chlorosilane method. However, in general, the existing methods are complicated, generate a significant amount of hazardous by-products, require a vacuum system, and are, therefore, quite expensive.

A number of new methods are under consideration for the purification of metallurgical-grade silicon (MG-Si), including: (1) repetitive porous MG-Si etching, gettering and surface-removal of impurities; (2) MG-Si gaseous melt-treatment; and (3) MG-Si purification by recrystallization of Si from MG-Si/metal solutions. Many of these potential methods improve upon the deficiencies of the existing techniques, yet most of the above-referenced techniques still contain some of the above-listed drawbacks, including specifically, the level of complexity of the processes used to generate consistent and predictable results, and which also increase the already high costs associated with producing pure feedstock products. Specifically, the porous silicon etch/gettering removal of impurities, although effective in the near surface region, appears impractical for bulk purification because of the large number of process cycles that would be required and that would thus drive up the time and cost needed to produce purified feedstock in sufficient quantities. The gaseous melt treatment using moist argon appears promising for reducing boron levels from the MG-Si source material, but requires much longer treatment times and more efficient exposure to the liquid silicon in order to

be cost-efficient at the level required for this specific problem. Finally, the recrystallization of silicon from MG-Si/metal solutions remains essentially theoretical at this time and is not the short-term solution needed to address current commercial concerns.

SUMMARY OF INVENTION

Accordingly, an object of the present invention is to provide a high deposition rate process for producing pure silicon feedstock from metallurgical-grade silicon.

Another object of the present invention is to provide a viable, economical and high through-put method of depositing pure silicon feedstock for solar cells and other applications.

Yet another object of the present invention is to provide an apparatus by which to produce pure silicon feedstock according to the method of the present invention.

Additional objects, advantages and novel features of the invention shall be set forth in part in the description that follows, and in part will become apparent to those skilled in the art upon examination of the following or may be learned by the practice of the invention. The objects and the advantages of the invention may be realized and attained by means of the instrumentalities and in combinations particularly pointed out in the appended claims.

To achieve the foregoing and other objects and in accordance with the purpose of the present invention, as embodied and broadly described herein, the method of this invention may comprise producing pure silicon feedstock by first placing solid metallurgical-grade silicon and solid iodine in the bottom portion of a cold-wall reactor, heating the bottom portion of the cold-wall reactor so as to create a thermal gradient while vaporizing the MG-Si and the iodine, which react chemically to produce SiI_2 precursor, drive a portion of the SiI_2 to a lower temperature and to thereby deposit the silicon upon a substrate within the cold-wall reactor chamber, and, by taking advantage of a variance in the partial pressures of the metal iodides vapors formed, separate the desirable iodides from the undesirable byproduct iodides by condensation of the desirable iodides on surfaces in the reaction chamber, capturing the iodide condensate in the reaction chamber, and transferring the condensate to a distillation chamber. In the distillation chamber, the condensate of desirable iodides is vaporized, and, once again taking advantage of a variance in the partial pressures of the metal iodide vapors formed to further separate residual undesirable iodide condensates from the desirable SiI_4 condensate, collect the SiI_4 condensate, and return it to the cold-wall reaction chamber for further cyclical processing until a desired quantity of pure silicon is deposited on the substrate within the cold-wall reactor chamber that it can be removed and replaced with a new substrate.

To produce feedstock using the method described herein, the apparatus of this invention may comprise a plurality of interconnected chambers that are at about atmospheric pressure. A first chamber may have a bottom portion, a mid-portion and a top portion, along with a plurality of inlets and a plurality of outlets. A second chamber may also have a bottom portion, a mid-portion and a top portion, as well as an inlet and a plurality of outlets. A third chamber may have an inlet and an outlet. The metallurgical-grade silicon may be deposited in the first chamber along with an amount of iodine source material. The bottom portion of the first chamber may be heated, thus producing a temperature gradient within the first chamber and also vaporizing a portion of the MG-Si and the I. Some of the vaporized

material will form SiI_2 which may be deposited upon a substrate in the mid-portion of the first chamber. Additionally, many byproduct metal iodide vapors will be formed, some of which will be separated and removed from the first chamber permanently and some of which will be separated and removed from the first chamber and transferred to the second chamber as liquid condensate.

The second chamber may also be heated, thus producing another temperature gradient and also vaporizing a portion of the liquid condensate. Some of the vaporized condensate will form a SiI_4 vapor which will be separated from other metal iodide vapors formed, collected, and transferred to a third chamber to be subsequently returned to the first chamber for re-use. The remaining undesirable metal iodide vapors formed will be separated and removed from the second chamber permanently. Other embodiments and variations based upon the above-described process and apparatus, as well as that which will be disclosed in more detail below, will be recognized by those persons skilled in the art.

BRIEF DESCRIPTION OF THE DRAWINGS

The accompanying drawings, which are incorporated herein and form a part of the specification illustrate preferred embodiments of the present invention, and together with the description, serve to explain the principles of the invention.

FIG. 1 is a cut-away schematic of the apparatus used to practice the process of the present invention.

FIG. 2 is a graph showing relative Iodide vapor pressures.

FIG. 3 is a graph showing impurity levels in the MG-Si source material and in an epitaxial silicon layer grown by the process and apparatus of the present invention.

FIG. 4 is a graph showing diagnostic solar cell parameters for a wafer from a crystal grown using ICVT-purified MG-Si produced by the process and apparatus of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

A pure silicon feedstock can be produced at high deposition rates and at low costs with the process and apparatus disclosed herein. Referring generally to FIG. 1, a silicon purification system 10 according to this invention has three interconnected chambers 20, 50, 80. In the first chamber 20, also called a cold-wall reactor chamber, solid pieces of metallurgical-grade silicon (MG-Si) 11 and iodine 12 are heated and evaporated in a bottom portion 21 of chamber 20 to create a vapor mixture of silicon and iodine, which react chemically to form SiI_2 gas. The SiI_2 gas rises to a slightly cooler region 22 in the chamber 20, where it goes through a disproportionation reaction to produce Si and SiI_4 . The Si deposits on a substrate 40, while the SiI_4 condenses on the interior wall 28 of the chamber 20, as indicated by droplets 13. The SiI_4 condensate 13 is collected by an annular catch ring 40 at the bottom portion of region 22 of chamber 20, which ring 40 routes the condensate 13 to a conduit 29 that is connected to a second chamber 50, which is also called a distillation chamber.

The MG-Si feedstock 11 also contains other elements, such as boron (B) and phosphorus (P), which also react with iodine to produce undesirable iodides, such as BI_3 and PI_3 . However, because they have different vapor pressures than the silicon iodides, these undesirable iodides do not enter into the SiI_2 disproportionation process described above, so the B and P do not deposit on the substrate 40. Instead, they

are substantially condensed and drawn off in a still cooler, top portion 23 of the reaction chamber 20, by an annular catch ring 41, as indicated by droplet 14 in conduit outlet 27. However, this separation process is not perfect, and some amount of BI_3 and PI_3 condenses below the outlet 27 in the mid-portion 22 of the reaction chamber 20, thus mixing with the SiI_4 condensate 13 that runs via conduit 29 into the distillation chamber 50. Other impurities, such as carbon tetraiodide (CI_4) may also be produced in the reaction chamber 20 and also mix with the SiI_4 condensate 13 and run via conduit 29 into the distillation chamber 50.

The purpose of the distillation chamber 50, therefore, is to further purify the SiI_4 by separating it from the undesirable iodides, e.g., BI_3 , PI_3 , CI_4 , and others. To do so, SiI_4 , BI_3 , PI_3 , CI_4 , and others mixed together in the pool 15 in the bottom portion 51 of the distillation chamber 50 are vaporized. The SiI_4 , BI_3 , PI_3 , and CI_4 vapors rise in the distillation chamber 50, where temperature decreases as distance from the bottom increases. The SiI_4 condenses at a higher temperature than BI_3 and PI_3 , so the SiI_4 condenses, as illustrated by droplets 16, in the mid-portion 52 and is drawn out of the distillation chamber 50 by an annular catch ring 42 and conduit 56. Meanwhile, the undesirable BI_3 and PI_3 condense at a cooler temperature in the top portion 53 of distillation chamber 50, as indicated by droplets 17, and is captured and drawn out of the distillation chamber 50 by an annular catch ring 43 and conduit 55. The CI_3 is condensed at a higher temperature in a lower portion of the distillation chamber 50, as indicated by droplets 18, and is captured and drawn out of chamber 50 by annular catch ring 44 and conduit 57.

Only the middle conduit 56, carrying the SiI_4 condensate 16 is connected to the third chamber or reservoir 80. Therefore, the reservoir 80 collects and holds the purified SiI_4 condensate 16. A feed tube 81 connects the reservoir 80 back to the bottom portion 21 of the reaction chamber 20, and a metering valve 82 meters the purified SiI_4 into the reaction chamber 20, where it is joined in the reaction cycle by combining with additional Si from the vaporized MG-Si feedstock 11 to produce more SiI_2 , which cools and disproportionates in mid-portion 22 to deposit more Si on the substrate 40 and produce more SiI_4 to be repurified in the distillation chamber 50, as described above. When a desired amount of pure Si is deposited on the substrate 40, the substrate 40 can be removed and replaced with new substrates 40.

With this overview of the silicon purification system 10 of this invention in mind, a more detailed explanation of the components and process steps is provided below. The reaction chamber 20, as mentioned above, has a bottom portion 21, a mid-portion 22 and a top portion 23. Cold-wall reactor chamber 20 further has a first inlet 24 through which metallurgical-grade silicon (MG-Si) source material 11 and iodine source material 12 are introduced into the chamber 20 and placed into the bottom portion 21. A purge line 25 may be connected to the system 10 through the first inlet 24 and is used initially to introduce gas (i.e. hydrogen) with which to drive all foreign vapors from the system 10 prior to operation. During operation, the purge line 25 is used to introduce a blanketing gas (i.e. hydrogen or any other blanketing gas that is less dense than, and non-reactive with, iodine vapor) with which to keep air out of the otherwise open system 10.

Heater 26 at least partially surrounds the bottom portion 21 of the chamber 20. Once MG-Si source material 11 and iodine source material 12 are introduced into the bottom portion 21 of the chamber 20, heat from heater 26 will be

applied to the bottom portion **21** of chamber **20** to vaporize a portion of both the MG-Si source material and the iodine source material. The heat applied by heater **26** will also create a temperature gradient to form within chamber **20**, such that the temperature T_0 at the bottom portion **21** of the chamber **20** is warmer than the temperature T_1 at the mid-portion **22** of the chamber **20**, which in turn is warmer than the temperature T_2 at the top portion **23** of the chamber. During the first stage of operation, the heater **26** initially applies enough heat to bring the temperature (T_0) at the bottom portion **21** of the chamber **20** to between 500° and 1000° C. At this range of temperatures, some silicon (Si) present in the MG-Si source material **11** will vaporize and react with a vapor of the iodine (I) source material **12** to form silicon tetraiodide (SiI_4) vapor and iodine (I) vapor. Several other impurities present in the MG-Si source material **11** (i.e., those impurities, e.g., boron (B), phosphorus (P), iron (Fe), and aluminum (Al), with free energies of formation with iodine greater in absolute value than that of silicon and iodine) will likewise react with the iodine source material **12** to form several impurity iodides (those impurities present in the MG-Si source material with free energies of formation with iodine less in absolute value than that of silicon and iodine will be retarded). The silicon tetraiodide (SiI_4) vapor and the several impurity iodide vapors (e.g., BI_3 and PI_3) are then driven upwardly through the mid-portion **22** of the chamber **20** and into the top portion **23** of the chamber **20**, where the lower temperature (T_2 is about 120° C.) causes some of the impurity iodide vapors (e.g., BI_3 and PI_3) to condense, as indicated by droplets **14**. The condensed impurity iodides **14** are then mostly collected at a first outlet **27** by annular catch ring **41** and drawn out of the reaction chamber **20** by way of a cold trap or such other mechanism that will be instantly recognized by and familiar to those persons skilled in the art, the details of which need not be further discussed herein.

The purer vapors, which include silicon tetraiodide (SiI_4) vapor, will condense on the interior wall **28** of the chamber **20**, as indicated by droplets **13**, at some point positioned lower than the first outlet **27**. It is important to keep the temperature (T_1) of the interior wall **28** "cold", i.e., the temperature T_1 of the interior wall **28** should be maintained between 120° and 700° C., in order to prevent any silicon deposition along the wall **28**. The condensate **13** of the purer vapors will run by gravity down the interior wall **28** of chamber **20** and will subsequently be collected by an annular catch ring **40** and transported out of chamber **20** through second outlet **29** and into second chamber **50**. Second chamber **50** is a distillation tower, which, similar to the cold-wall reactor chamber **20**, has a bottom portion **51**, a mid-portion **52** and a top portion **53**, and a first outlet **55**, a second outlet **56** and a third outlet **57**. The bottom portion **51** is at least partially surrounded by heater **54**, which will heat the bottom portion **51** of chamber **50** to a temperature (T_3) of about 310° C. Similar to the temperature gradient formed by heater **26** in chamber **20**, a temperature gradient is formed in chamber **50** such that the temperature (T_4) at the first outlet **55** is lower than the temperature (T_5) at the second outlet, which is lower than the temperature (T_6) at the third outlet, which is lower than T_3 .

Referring to FIG. 2, it is shown that most of the potential impurity iodides (i.e., FeI_2 , AlI_3 , etc.) have vapor pressures lower than the vapor pressure of silicon tetraiodide, thus those potential impurity iodides will remain in the liquid mix **15** in the bottom portion **51** of the chamber, while boron triiodide, phosphorus triiodide and carbon tetraiodide, that have higher partial pressures than silicon tetraiodide, will

vaporize along with silicon tetraiodide at temperature T_3 and at about atmospheric pressure. As can be seen in FIG. 2, at one atmosphere, boron triiodide and phosphorus triiodide boil at about 63° C. lower than silicon tetraiodide, and carbon tetraiodide boils at about 19° C. higher than silicon tetraiodide.

Thus, the three outlets **55**, **56**, **57** of chamber **50** of the preferred embodiment are positioned such that first outlet **55** is positioned in the top portion **53** of chamber **50** at temperature T_4 , the second outlet **56** is positioned below first outlet **55** at a temperature T_5 , and third outlet **57** is positioned below second outlet **56** but above the bottom portion **51** of chamber **50** and is at temperature T_6 . Upon the application of heat by heater **54** to the bottom portion **51** of chamber **50**, the silicon tetraiodide and the other impurity iodides are vaporized and driven upwardly through the chamber **50**. At the first outlet **55**, temperature T_4 is about 120° C. and the vaporized impurity iodides that have lower boiling points than silicon tetraiodide vapor (i.e. BI_3 and PI_3) condense, as is indicated by droplets **17**, and are collected by annular catch ring **43** and removed from chamber **50** at a cold trap similar to the way that the impurity iodides are trapped in, and removed from, the cold-wall reaction chamber **20**, as disclosed above. Similarly, at the second outlet **56**, temperature T_5 is about 180° C., the temperature at which silicon tetraiodide condenses as shown by droplets **16**. Condensed silicon tetraiodide **16** is collected by annular catch ring **42** and removed from chamber **50** via second outlet **56**, which is connected to chamber **80**, which in the preferred embodiment, is a reservoir used to temporarily store liquid silicon tetraiodide **16**. Lastly, third outlet **57** is maintained at temperature T_6 at about 205° C., the temperature at which carbon tetraiodide is condensed, as illustrated by droplets **18**, collected by annular catch ring **44**, and removed at a cold trap in the same manner as has been previously discussed.

At this stage of the operating cycle, the purified silicon tetraiodide **16** that has been collected in chamber **80**, is returned to chamber **20** via outlet **81** through the opening of valve **82**. When the purified liquid silicon tetraiodide **16** collects in the bottom portion **21** of chamber **20**, the heat applied to bottom portion **21** is increased to a temperature (T_0) in excess of 1000° C., and preferably in the range of 1000° to 1400° C. At temperature T_0 , the purified silicon tetraiodide (SiI_4) **16** further reacts with the still-present silicon from the MG-Si source material **11** to form silicon diiodide (SiI_2) vapor. The silicon diiodide vapor is very unstable and, as the vapor is driven upwardly into the mid-portion **22** of chamber **20**, the chemical reaction, $\text{SiI}_2 \rightarrow \text{Si} + \text{SiI}_4$, drives the disproportionation of SiI_2 and the deposition of silicon (Si) onto substrate(s) **40**. Other metal iodides (i.e., AlI_3 , etc.) have very large and negative values of free energy of formation, and while they will form vapors readily, within the deposition zone, they exhibit a very small tendency to be reduced and thus the silicon deposition on the substrate(s) **40** is quite pure. Substrate(s) **40** are preferably high purity silicon slim rods or tubes or carbon tubes or rods, and are heated by heater **30** to a temperature (T_s) of about 750° C. The temperature T_f is continuously applied to bottom portion **21** of chamber **20** for the remainder of the cycle. The silicon tetraiodide vapor and the other metal impurity iodide vapors generated by the secondary reaction at temperature T_f go through the distillation process as described above for a second (or third, fourth, etc) time before again returning as purified silicon tetraiodide **16** from outlet **81** of reservoir **80** to the bottom portion **21** of chamber **20**.

The replenishment of MG-Si and iodine source materials 11, 12 is accomplished through inlet 24 of chamber 20 along with a purging gas flow at the opening 25, and the volatile gases are kept in the system 10 by a blanketing cloud layer due to the condensation of iodine vapor plus the gravity effect as described in detail in U.S. patent application Ser. No. 09/334,166, filed on Jun. 15, 1999 by the applicants and assigned to the same entity and incorporated herein by reference. The ability to replenish the source materials, recycle byproducts, and continuously load and unload substrate(s) 40 gives the above-described process and apparatus significant cost advantages over existing and previously disclosed silicon purification systems. Further, the fact that the system 10 is an open system that operates at about atmospheric pressure eliminates the need to incorporate expensive vacuum equipment into the manufacturing cycle, further reducing total system cost. Finally, the disclosed system 10 can be modified by increasing the number of chambers to potentially include separate chambers for doping silicon feedstock and can likewise be modified by changing the number of outlets and the relative temperatures to specifically target particular impurities with defined partial pressures, vaporization points and condensation points.

The above-described purification technique and apparatus provided example results as follows. With a source silicon temperature (T_s) >1200° C. and a substrate temperature (T_s) of about 1000° C., a purified silicon deposition rate >5 $\mu\text{m}/\text{min}$ was achieved. The resultant single-crystal substrates were approximately 100 μm -thick epitaxial silicon layers. Impurity levels in the layers were analyzed by secondary ion mass spectrometry (SIMS) and glow discharge mass spectroscopy (GDMS) and the results are shown in FIG. 3. Specifically, the graph shows the measured initial impurity level of the metallurgical-grade silicon which is denoted by a circular dot. The allowable solar-grade silicon (SoG-Si) content range is denoted by two connected squares, with each square representing the minimum and maximum level of each impurity necessary to meet the minimum purity requirements for SoG-Si. The triangular marks denote the impurity level results generated by the ICVT technique described above as measured by GDMS, and the diamond-shaped marks denote the same results as measured by the SIMS. With the exception of boron (and phosphorus which is not shown), all results produced by the method and apparatus disclosed by the present invention, show reductions by several orders of magnitude and are within the target ranges. And with the addition of the distillation chamber 50 to the system 10, the levels of boron (and phosphorus) would be reduced to within the allowable SoG-Si range as well.

A second experiment was conducted using multiple large area substrates for ICVT growth of thick layers that were harvested and melted as feedstock for Czochralski (CZ) crystal growth and analysis. All major impurities were greatly reduced as shown by Table 1 below:

Element	CZ-Si from ICVT (ppma)	MG-Si source (ppma)
B	4.157	14.548
C	14.264	107.565
O	17.554	66.706
Mg	<0.001	8.204
Al	<0.005	520.458
Si	matrix	matrix
P	6.801	21.762

-continued

Element	CZ-Si from ICVT (ppma)	MG-Si source (ppma)
S	<0.044	0.096
K	<0.007	<0.036
Ca	<0.007	44.849
Ti	<0.001	47.526
V	<0.001	143.345
Cr	<0.001	19.985
Mn	<0.001	19.938
Fe	<0.005	553.211
Co	<0.002	0.763
Ni	<0.002	22.012
Cu	<0.001	1.724
Zn	<0.002	0.077
As	<0.002	0.007
Sr	<0.0003	0.353
Zr	<0.0003	2.063
Mo	<0.001	0.790
I	<0.0002	<0.001
Ba	<0.0002	0.266
W	<0.0003	0.024

All the metal impurities, as illustrated above, were below the detection limits of the GDMS technique. The resultant crystal created diagnostic solar cells with efficiencies of 9.5% and voltage v. current density characteristics as illustrated by the graph in FIG. 4. Thus, the ICVT technique disclosed and illustrated herein, along with the apparatus described above and claimed below, generated purified silicon feedstock consistently and predictably, at fast deposition rates and at low operating costs.

The foregoing is considered as illustrative only of the principal of the invention. Further, since numerous modifications and changes will occur to those persons skilled in the art, it is not desired to limit the invention to the exact construction and operation shown and described, and accordingly all suitable modifications and equivalents may be resorted to falling within the scope of the invention as defined by the claims which follow.

What is claimed is:

1. A system for purifying metallurgical-grade silicon and depositing the purified silicon on a substrate, comprising:
 - a first chamber, the first chamber further comprising a bottom portion, a mid-portion and a top portion, a first inlet, a purge gas line, a first outlet positioned in the top portion, a second outlet positioned lower than the first outlet, a second inlet positioned below the second outlet, a first heater at least partially surrounding the bottom portion, the first heater selectively varying the amount of heat applied to the bottom portion, and a second heater at least partially surrounding a portion of the first chamber positioned below the first outlet and above the second inlet;
 - a second chamber, the second chamber further comprising a bottom portion, a mid-portion and a top portion, an inlet which is in fluid communication with, and is interconnected with the second outlet of the first chamber, a first outlet positioned in the top portion of the second chamber, a second outlet positioned below the first outlet in the second chamber, a third outlet positioned below the second outlet of the second chamber but above the bottom portion of the second chamber, and a heater at least partially surrounding the bottom portion of the second chamber; and
 - a third chamber, the third chamber comprising an inlet, the inlet in fluid communication with, and interconnected with the second outlet of the second chamber, and an outlet, the outlet in fluid communication with, and interconnected with the second inlet of the first chamber.

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- 2. The system of claim 1, the first chamber further comprising a substrate disposed vertically within the portion of the first chamber positioned below the first outlet of the first chamber and above the second inlet of the first chamber.
- 3. The system of claim 1, the first chamber further comprising a substrate disposed horizontally within the portion of the first chamber positioned below the first outlet of the first chamber and above the second inlet of the first chamber.
- 4. The system of claim 2 or claim 3, the first chamber comprising more than one substrate disposed within the

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- portion of the first chamber positioned below the first outlet of the first chamber and the second inlet of the first chamber.
- 5. The system of claim 1, the first outlet of the first chamber, the first outlet of the second chamber and the third outlet of the second chamber further comprising a cold trap.
 - 6. The system of claim 1, the third chamber further comprising a valve by which to control the flow from the third chamber to the first chamber.

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